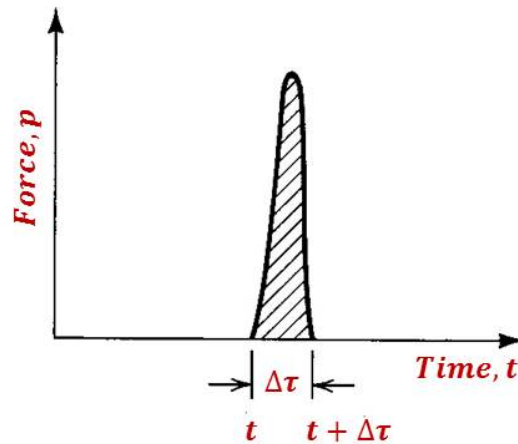


RESPONSE TO GENERAL DYNAMIC LOADING

The time integral of a force is referred to as **impulse**, is determined by I and is obtained from:

$$I = \int_t^{t+\Delta t} p(t) dt$$

Newton's 2nd Law of motion states that **the action of an (impulsive) force on a mass, results in a change in the velocity of the mass and hence in its linear momentum, the change in linear momentum being equal to the impulse of the (impulsive) force.**

Thus, representing the change in velocity by $\Delta\dot{u}$,

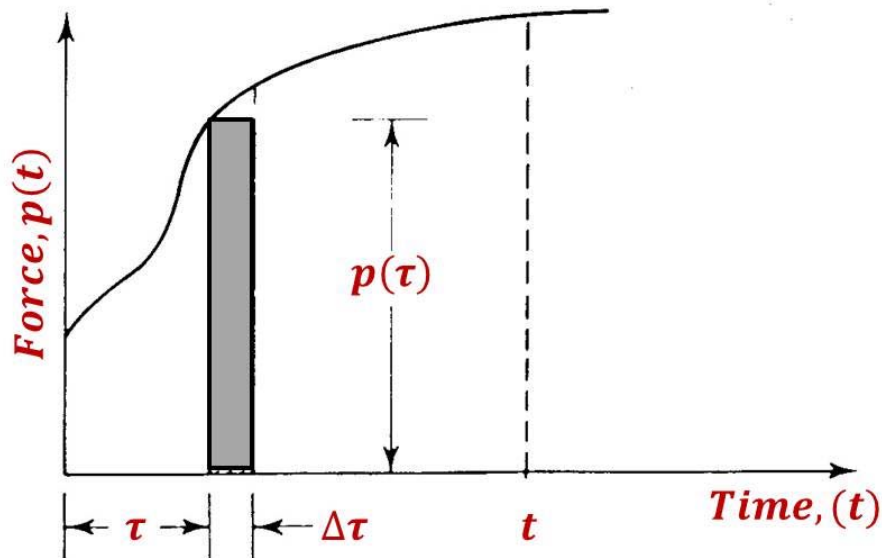
$$m\Delta\dot{u} = I$$

If the mass is **initially at rest**, it will have a velocity (I/m) after the action of the impulse.

Suppose that a SDOF system is subjected to an impulse $I = p(\tau) \cdot \Delta\tau$. The action of the impulse will set the system vibrating. **The ensuing free vibration response can be obtained by recognizing that the initial displacement is zero and the initial velocity is (I/m) .**

Thus, the resulting response is:

$$u(t) = \frac{I}{m\omega_d} e^{-\xi\omega t} \sin(\omega_d t) = I \cdot h(t)$$



We approximate the general loading $p(t)$ by a series of pulses of intensity $p(t) \cdot \Delta\tau$.

Hence, a pulse applied at time τ contributes to the response at time t an amount equal to:

$$\Delta u(t) \cong [p(\tau)\Delta\tau] \cdot h(t - \tau)$$

where: $h(t) = \frac{1}{m\omega_d} e^{-\xi\omega t} \sin(\omega_d t)$ (= **unit impulse response function**)

The above expression is approximate when $\Delta\tau$ is finite but becomes exact as $\Delta\tau \rightarrow 0$.

Thus, the contribution of all the pulses ($0 \leq \tau \leq t$) is given by:

$$u(t) \cong \sum \{p(\tau)\Delta\tau \cdot h(t - \tau)\}$$

At the limit as $\Delta\tau \rightarrow 0$, we obtain:

$$u(t) = \int_0^t p(\tau)h(t - \tau) d\tau$$

We can obtain the **unit impulse response** $h(t)$ using the **Dirac (delta) function** $\delta(t)$:

Equation of Motion:

$$m\ddot{u} + c\dot{u} + ku = I\delta(t) \quad [I = \text{impulse intensity}]$$

$$\Rightarrow \ddot{u} + 2\xi\omega\dot{u} + \omega^2u = \left(\frac{I}{m}\right)\delta(t)$$

$$\text{UNITS: } \begin{cases} [I] & = [F][T] \\ [\delta(t)] & = [T]^{-1} \end{cases}$$

Initial conditions: $u(0^-) = 0$ & $\dot{u}(0^-) = 0$ (i.e., system at rest)

Integrate the Equation of Motion formally over $(-\varepsilon, +\varepsilon)$ and take the limit as $\varepsilon \rightarrow 0$:

$$\lim_{\varepsilon \rightarrow 0} \left\{ \int_{-\varepsilon}^{+\varepsilon} \ddot{u}(t) dt + 2\xi\omega \int_{-\varepsilon}^{+\varepsilon} \dot{u}(t) dt + \omega^2 \int_{-\varepsilon}^{+\varepsilon} u(t) dt = \left(\frac{I}{m}\right) \int_{-\varepsilon}^{+\varepsilon} \delta(t) dt \right\}$$

$$\lim_{\varepsilon \rightarrow 0} \left\{ [\dot{u}(+\varepsilon) - \dot{u}(-\varepsilon)] + 2\xi\omega [u(+\varepsilon) - u(-\varepsilon)] + \omega^2 \underbrace{\int_{-\varepsilon}^{+\varepsilon} u(t) dt}_0 = \left(\frac{I}{m}\right) \right\}$$

$$\left[\dot{u}(0^+) - \underbrace{\dot{u}(0^-)}_0 \right] + 2\xi\omega \underbrace{[u(0^+) - u(0^-)]}_0 + 0 = \left(\frac{I}{m}\right)$$

$\therefore u(t) = \text{continuous}$

Therefore:

$$\boxed{\dot{u}(0^+) = \left(\frac{I}{m}\right)}$$

Therefore, we can make the following statement:

$$\left. \begin{array}{l} m\ddot{u} + c\dot{u} + ku = I\delta(t) \\ u(0^-) = 0 \quad \& \quad \dot{u}(0^-) = 0 \end{array} \right\} \text{equivalent} \left\{ \begin{array}{l} m\ddot{u} + c\dot{u} + ku = 0 \quad (t > 0) \\ \dot{u}(0) = \left(\frac{I}{m}\right) \quad \& \quad u(0) = 0 \end{array} \right.$$

Therefore, the effect of the impulsive force $p(t) = I\delta(t)$ is to impart to the SDOF system an initial velocity equal to (I/m) .

The response of the SDOF system governed by:

Equation of Motion: $m\ddot{u} + c\dot{u} + ku = 0 \quad (t > 0)$

Initial Conditions: $\dot{u}(0) = \left(\frac{I}{m}\right) \quad \& \quad u(0) = 0$

is given by:

$$\begin{aligned} u(t) &= e^{-\xi\omega t} \left[u(0) \cos(\omega_d t) + \frac{\dot{u}(0) + \xi\omega u(0)}{\omega_d} \sin(\omega_d t) \right] \\ &= \frac{(I/m)}{\omega_d} e^{-\xi\omega t} \sin(\omega_d t) \end{aligned}$$

For $I = 1$, the above response is denoted by $h(t)$ and is referred to as the unit impulse response function.

Therefore:

$$\begin{array}{l} 1 \cdot \delta(t) \rightarrow \boxed{\text{SDOF}}_{(\xi = 0)} \rightarrow h(t) = \frac{1}{m\omega} \sin(\omega t) \\ 1 \cdot \delta(t) \rightarrow \boxed{\text{SDOF}}_{(0 < \xi < 1)} \rightarrow h(t) = \frac{1}{m\omega_d} e^{-\xi\omega t} \sin(\omega_d t) \end{array}$$

Assuming that we know the unit impulse response of the **system/structure**, the response integral $u(t) = \int_0^t p(\tau)h(t - \tau) d\tau \stackrel{\text{def}}{=} p(t) * h(t)$ may be derived also using a '**Linear Systems Theory**' approach.

Sifting property of the Dirac (delta) function $\delta(t)$:

$$\int_{-\infty}^{+\infty} \delta(t - t_0)f(t) dt = f(t_0)$$

NOTE: The verb '**to sift**' means **to put through a sieve**.

EXCITATION		RESPONSE
$\delta(t)$	\rightarrow SDOF \rightarrow	$h(t) = \frac{1}{m\omega_d} e^{-\xi\omega t} \sin(\omega_d t)$
$\delta(t - \tau)$	\rightarrow SDOF \rightarrow	$\underbrace{h(t - \tau)}_{\text{time-invariant system}}$
$\delta(t - \tau)p(\tau)d\tau$	\rightarrow SDOF \rightarrow	$\underbrace{h(t - \tau)p(\tau)d\tau}_{\text{linear system}}$
$\underbrace{\int_0^{+\infty} \delta(t - \tau)p(\tau)d\tau}_{\text{sifting property of } \delta(t)}$	\rightarrow SDOF \rightarrow	$\underbrace{\int_0^t h(t - \tau)p(\tau)d\tau}_{\text{superposition}}$
$p(t)$	\rightarrow SDOF \rightarrow	$u(t) = \int_0^t h(t - \tau)p(\tau)d\tau$

Therefore, **the response of the SDOF system** to an **arbitrary loading $p(t)$** , **starting from rest**, is given by:

$$u(t) = \int_0^t p(\tau)h(t - \tau) d\tau \quad \left(\begin{array}{c} \text{convolution} \\ \text{or} \\ \text{Duhamel's} \\ \text{integral} \end{array} \right)$$

The above integral is known as the '**convolution integral**' or '**Duhamel's integral**'.

If the SDOF system **starts from a state other than the state of rest**, then the response is given by:

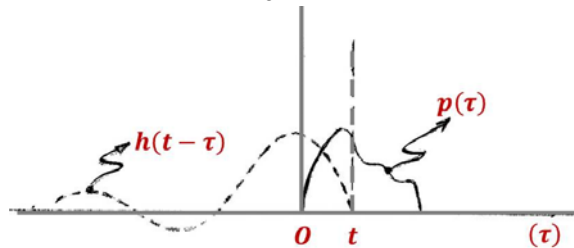
$$u(t) = e^{-\xi\omega t} \left[u(0) \cos(\omega_d t) + \frac{\dot{u}(0) + \xi\omega u(0)}{\omega_d} \sin(\omega_d t) \right] + \int_0^t p(\tau)h(t - \tau) d\tau$$

Note the following properties of the convolution integral:

$$u(t) = p(t) * h(t) \stackrel{\text{def}}{=} \int_0^t p(\tau)h(t - \tau) d\tau$$

$$= \int_0^t p(t - \xi)h(\xi) d\xi$$

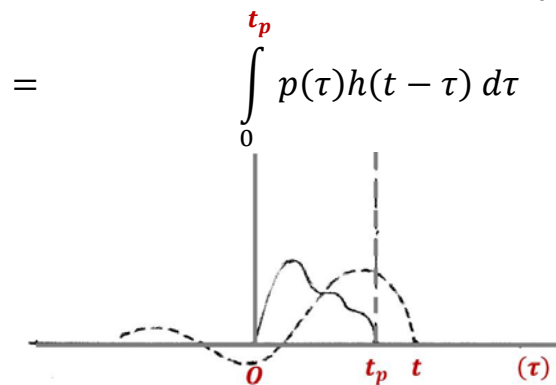
Graphical representation of $\int_0^t p(\tau)h(t - \tau) d\tau$:



Note that when t is greater than the pulse time, say t_p , then:

$$u(t) = \int_0^t p(\tau)h(t - \tau) d\tau$$

$$= \int_0^{t_p} p(\tau)h(t - \tau) d\tau + \underbrace{\int_{t_p}^t p(\tau)h(t - \tau) d\tau}_0$$



Considering that for $t > t_p$ the load application ceases, **the oscillator will perform free vibrations with initial conditions $u(t_p)$ & $\dot{u}(t_p)$** . The integral $\int_0^{t_p} p(\tau)h(t - \tau) d\tau$ expresses/evaluates these free oscillations.

NOTE:

Let an **Initial Value Problem (IVP)** be specified by the following n^{th} order **linear Ordinary Differential Equation (ODE)** with constant coefficients:

$$a_n \frac{d^n u}{dt^n} + a_{n-1} \frac{d^{n-1} u}{dt^{n-1}} + \dots + a_0 u = r(t)$$

Let the **associated linear operator**:

$$L[] = a_n \frac{d^n}{dt^n} + a_{n-1} \frac{d^{n-1}}{dt^{n-1}} + \dots + a_0$$

Then, the **Green's function $G(t)$** of the above linear differential operator $L[]$ with constant coefficients is the function that satisfies:

(i) The homogeneous ODE:

$$L[G] = 0$$

(ii) The initial conditions:

$$G(0) = \frac{dG(0)}{dt} = \frac{d^2 G(0)}{dt^2} = \dots = \frac{d^{n-2} G(0)}{dt^{n-2}} = 0 \quad \& \quad \frac{d^{n-1} G(0)}{dt^{n-1}} = \frac{1}{a_n}$$

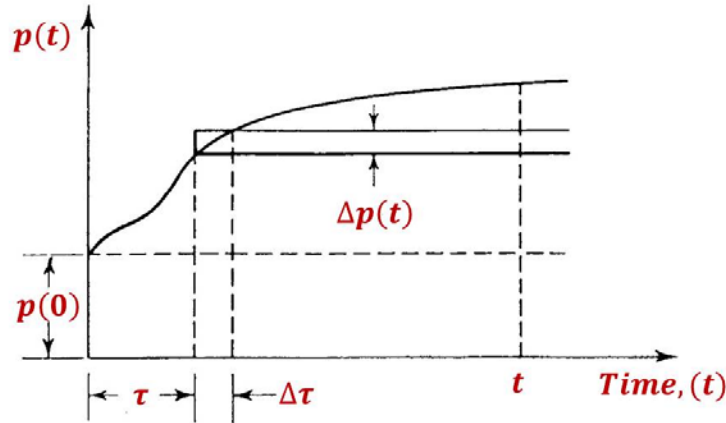
It can be demonstrated that:

$$u(t) = \int_0^t r(\tau) G(t - \tau) d\tau$$

is a solution of the above inhomogeneous ODE.

It is now evident that the unit impulse response $h(t)$ is the Green's function of the equation of motion.

**Derivation Of Duhamel's (Convolution) Integral
Using the Response to a Force Described by the Unit Step Function**



Let $g(t)$ be the **displacement response of a SDOF system, starting from rest, to a force described by the unit step function $\mathbb{H}(t)$** , i.e., $p(t) = p_0 \cdot \mathbb{H}(t) = 1 \cdot \mathbb{H}(t)$. Specifically,

$$g(t) = \frac{1}{k} \left\{ 1 - e^{-\xi\omega t} \left[\cos(\omega_d t) + \frac{\xi}{\sqrt{1-\xi^2}} \sin(\omega_d t) \right] \right\}, \quad t \geq 0$$

NOTE: The above result may be obtained by considering the governing equation of motion $m\ddot{u} + c\dot{u} + ku = p(t)$, where $p(t) = p_0 \cdot \mathbb{H}(t) = 1 \cdot \mathbb{H}(t)$, subject to initial conditions: $u(t=0) = 0$ & $\dot{u}(t=0) = 0$. The general solution of the above equation is written as follows: $u(t) = u_H(t) + u_p(t) = e^{-\xi\omega t} [A \cos(\omega_d t) + B \sin(\omega_d t)] + (1/k)$. After imposing the given initial conditions, we obtain the above (boxed) result.

Contribution to the response of a step function of amplitude $\Delta p(t, \tau)$ applied at $t = \tau$:

$$\Delta u(t, \tau) \cong \Delta p(\tau) g(t - \tau) = \frac{\Delta p(\tau)}{\Delta \tau} g(t - \tau) \Delta \tau$$

Therefore:

$$u(t) \cong p(0)g(t) + \sum \left\{ \frac{\Delta p(\tau)}{\Delta \tau} g(t - \tau) \Delta \tau \right\}$$

As $\Delta \tau \rightarrow 0$, we obtain:

$$u(t) = p(0)g(t) + \int_0^t \frac{dp(\tau)}{d\tau} g(t - \tau) d\tau \quad \text{Duhamel's integral}$$

Integrating by parts:

$$\begin{aligned} u(t) &= p(0)g(t) + g(t-\tau)p(\tau)|_0^t - \int_0^t p(\tau) \frac{dg(t-\tau)}{d\tau} d\tau \\ &= g(0)p(t) + \int_0^t p(\tau) \frac{dg(t-\tau)}{dt} d\tau \end{aligned}$$

Applying **Leibnitz rule** for **differentiation under the integral sign**, we obtain:

$$u(t) = \frac{d}{dt} \int_0^t g(t-\tau)p(\tau) d\tau$$

NOTE: LEIBNITZ RULE

Let:
$$I(\varepsilon) = \int_{x_1(\varepsilon)}^{x_2(\varepsilon)} f(x, \varepsilon) dx$$

Then:
$$\frac{dI}{d\varepsilon} = f(x_2, \varepsilon) \frac{dx_2}{d\varepsilon} - f(x_1, \varepsilon) \frac{dx_1}{d\varepsilon} + \int_{x_1(\varepsilon)}^{x_2(\varepsilon)} \frac{\partial f(x, \varepsilon)}{\partial \varepsilon} dx$$

It is straightforward to show that:

$$h(t) = \frac{d}{dt} g(t)$$

Indeed,

$$\begin{aligned} \frac{dg(t)}{dt} &= \frac{d}{dt} \left\{ \frac{1}{k} - \frac{e^{-\xi\omega t}}{k} \left[\cos(\omega_D t) + \frac{\xi}{\sqrt{1-\xi^2}} \sin(\omega_D t) \right] \right\} \\ \left\{ \begin{aligned} &\frac{\xi\omega}{k} e^{-\xi\omega t} \left[\cos(\omega_D t) + \frac{\xi}{\sqrt{1-\xi^2}} \sin(\omega_D t) \right] \\ &+ \\ &-\frac{1}{k} e^{-\xi\omega t} [-\omega_D \sin(\omega_D t) + \xi\omega \cos(\omega_D t)] \end{aligned} \right\} &= \frac{e^{-\xi\omega t}}{k} \sin(\omega_D t) \left[\frac{\xi^2 \omega}{\sqrt{1-\xi^2}} + \omega_D \right] \\ \frac{e^{-\xi\omega t}}{k} \sin(\omega_D t) \frac{\omega}{\sqrt{1-\xi^2}} &= \frac{e^{-\xi\omega t}}{m\omega_D} \sin(\omega_D t) \end{aligned}$$

EXAMPLE:

Let the SDOF system of mass m and stiffness k be subjected to a loading $p(t)$, where:

$$p(t) = \begin{cases} p_0 & t \leq t_d \\ 0 & t > t_d \end{cases}$$

Compute the displacement response of the SDOF system using the convolution integral; assume that the system responds to the applied load starting from rest.

Solution:

The unit impulse response for the undamped SDOF system is: $h(t) = \frac{1}{m\omega} \sin(\omega t)$. Therefore:

$$\begin{aligned} \frac{h(t) * p(t)}{u(t)} &= \begin{cases} \int_0^t \frac{1}{m\omega} \sin[\omega(t-\tau)] \cdot p(\tau) d\tau & t \leq t_d \\ \int_0^{t_d} \frac{1}{m\omega} \sin[\omega(t-\tau)] \cdot p(\tau) d\tau & t > t_d \end{cases} \\ &= \begin{cases} \frac{1}{m\omega^2} \cdot [1 - \cos(\omega t)] & t \leq t_d \\ \frac{1}{m\omega^2} \cdot [\cos(\omega(t-t_d)) - \cos(\omega t)] & t > t_d \end{cases} \end{aligned}$$

Details of the evaluation of the convolution integral (two phases):

$$\begin{aligned} \int_0^t \frac{1}{m\omega} \sin[\omega(t-\tau)] \cdot p(\tau) d\tau &= \frac{1}{m\omega} \cdot \int_0^t \sin[\omega(t-\tau)] \cdot 1 d\tau \stackrel{\xi=t-\tau}{\cong} \frac{1}{m\omega} \cdot \int_t^0 \sin[\omega\xi] d(-\xi) \\ &= \frac{1}{m\omega} \cdot \int_0^t \sin[\omega\xi] d\xi \stackrel{\zeta=\omega\xi}{\cong} \frac{1}{m\omega^2} \cdot \int_0^{\omega t} \sin \zeta d\zeta \\ &= \frac{1}{m\omega^2} \cdot (-\cos \zeta)|_0^{\omega t} = \frac{1}{m\omega^2} \cdot [1 - \cos(\omega t)] \\ \\ \int_0^{t_d} \frac{1}{m\omega} \sin[\omega(t-\tau)] \cdot p(\tau) d\tau &= \frac{1}{m\omega} \cdot \int_0^{t_d} \sin[\omega(t-\tau)] \cdot 1 d\tau \stackrel{\xi=t-\tau}{\cong} -\frac{1}{m\omega} \cdot \int_t^{t-t_d} \sin[\omega\xi] d\xi \\ &= -\frac{1}{m\omega^2} \cdot \int_{\omega t}^{\omega(t-t_d)} \sin \zeta d\zeta = \frac{1}{m\omega^2} \cdot \cos \zeta \Big|_{\omega t}^{\omega(t-t_d)} \\ &= \frac{1}{m\omega^2} \cdot [\cos(\omega(t-t_d)) - \cos(\omega t)] \end{aligned}$$

PART (06): RESPONSE TO GENERAL DYNAMIC LOADING

From the result we obtained above for $u(t) = h(t) * p(t)$ by calculating the convolution integral for the time interval $t \leq t_d$, we may calculate the following quantities:

$$u(t_d) = \frac{1}{m\omega^2} \cdot [1 - \cos(\omega t_d)]$$

$$\dot{u}(t_d) = \frac{1}{m\omega} \cdot \sin(\omega t_d)$$

Consider the response of the oscillator for $t > t_d$, i.e., **after the load application has ceased**. The oscillator performs **free vibration oscillations** with initial conditions $u(t_d)$ & $\dot{u}(t_d)$. Specifically,

$$\begin{aligned} u(t) &= u(t_d) \cos(\omega(t - t_d)) + \frac{\dot{u}(t_d)}{\omega} \sin(\omega(t - t_d)) \\ &= \frac{1}{m\omega^2} \cdot [[1 - \cos(\omega t_d)] \cos(\omega(t - t_d)) + \sin(\omega t_d) \sin(\omega(t - t_d))] \\ &= \frac{1}{m\omega^2} \cdot [\cos(\omega(t - t_d)) - \cos(\omega t_d) \cos(\omega(t - t_d)) + \sin(\omega t_d) \sin(\omega(t - t_d))] \\ &= \frac{1}{m\omega^2} \cdot [\cos(\omega(t - t_d)) - \cos(\omega t)] \end{aligned}$$

The last expression is indeed what we obtained by evaluating the convolution integral for $t > t_d$.